

Analysis of 802.11 OFDM in High Multipath Environments

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Abstract—The performance loss of 802.11 OFDM systems due to propagation delay spread has been analyzed as a function of OFDM parameters for a wide range of reverberation times. This analysis results into solutions for the OFDM design to suppress the performance degradation.

Index Terms—delay spread; diffuse multipath; reverberation time; OFDM; room electromagnetics

I. INTRODUCTION

The performance of OFDM (orthogonal frequency-division multiplexing) systems can be degraded by the signal distortion over the FFT (fast Fourier transform) window caused by the propagation delay spread. In [1], we proposed to describe this effect in narrowband OFDM systems (such as IEEE 802.11a/g/n/ac) by an additive white Gaussian noise (AWGN) noise, characterized by a noise factor F_{delay} . This effect originates from replicas of the transmitted OFDM pulse with a delay larger than the cyclic prefix length CP . The intensity of these propagation paths can be high, especially in indoor environments, resulting into intersymbol and intercarrier (ISI/ICI) interference. For delays higher than CP , the channel typically consists of diffuse multipath components only. Here, the theory of room electromagnetics is applicable [2], according to which the averaged power delay profile (APDP) decays exponentially. This APDP decay is characterized by the time constant τ_r , referred to as the reverberation time, and the intensity parameter I_{diff} [Hz] [1]. As P_0 , the APDP power coefficient of first arriving path, is dependent on the frequency width Δf_0 of the Hann window applied to obtain the APDP, the intensity of the diffuse field will be expressed by the physical parameter I_{diff} , defined by $I_{diff} = P_0 \Delta f_0$ [1]. Based on this theory, an analytical expression of F_{delay} has been developed in [1] in terms of OFDM parameters and the propagation parameters τ_r and I_{diff} .

In this work, a parametric analysis of F_{delay} is carried out as a function of OFDM parameters, based on the aforementioned analytical expression for F_{delay} . This analysis is done for typical IEEE 802.11a/g/n/ac parameters [3] [4]. This gives insight and solutions for the OFDM design to suppress the performance loss due to the propagation delay spread.

II. DETERMINATION OF F_{delay}

In [1], the performance loss due to the signal distortion over the FFT window (caused by the propagation delay spread),

described by a loss factor L_{delay} , has been related to the noise factor F_{delay} as follows:

$$L_{delay} = 1 + \frac{F_{delay}}{F_{lin} IL_{lin}}, \quad (1)$$

where F_{lin} and IL_{lin} are the conventional (linear-scaled) noise factor and implementation loss of the receiver, resp. (i.e., corresponding to the situation where receiver and transmitter are connected by a cable). Therefore, our analysis will be done in terms of F_{delay} .

For the purpose of this work, we rewrite the expression for F_{delay} from [1] as a function of the following relevant OFDM design parameters: the transmit power per frequency unit $P_{T,f}$, the total bandwidth BW of the channel, the FFT period P , CP and the sampling factor f_s . The number of samples per FFT period (N_{sample}) is typically higher or equal than the total number of subcarriers, being $BW \times P$. N_{sample} is usually expressed by means of the sampling factor f_s :

$$N_{sample} = f_s BWP. \quad (2)$$

III. PARAMETRIC ANALYSIS

In this section, the analytical estimation for F_{delay} is analyzed as a function of P , CP , BW and f_s . All calculations of F_{delay} presented in this work are, unless otherwise mentioned, based on the 802.11a physical standard: $P = 3.2 \mu s$, $CP = 800$ ns, $BW = 20$ MHz and $f_s = 1$. We assume a typical value for I_{diff} of 6 Hz and a wide range of τ_r varying from 10 ns to 200 ns, based on experimental results [1]. For our calculations, we assume $P_{T,f} = 6.2 \cdot 10^{-9}$ W/Hz, based on a 20 dBm transmit power. For a 30 dBm transmit power, F_{delay} can be simply found as 10 dB higher, as F_{delay} is proportional to the transmit power [1].

A. Influence of the cyclic prefix duration CP

In Fig. 1, F_{delay} is shown as a function of CP for different τ_r . F_{delay} decreases strongly with increasing CP , due to the fact that F_{delay} is proportional to $\exp(-CP/\tau_r)$. Although the dependency of F_{delay} on CP is less strong for higher τ_r , increasing CP still provides an efficient strategy to reduce the interference due to delay spread. E.g., for $\tau_r = 140$ ns, F_{delay} decreases from 28.6 dB to 3.8 dB when switching from an 800 ns CP to 1600 ns. This corresponds to a loss L_{delay} reduction of about 14 dB (see (1)). For a 30 dBm transmit power, the decrease of F_{delay} is even from 38.6 dB to 13.8 dB. When switching from an 800 ns CP to 1600 ns, the

data rate is reduced with about 17%. However, this is largely compensated by the strong reduction of L_{delay} .

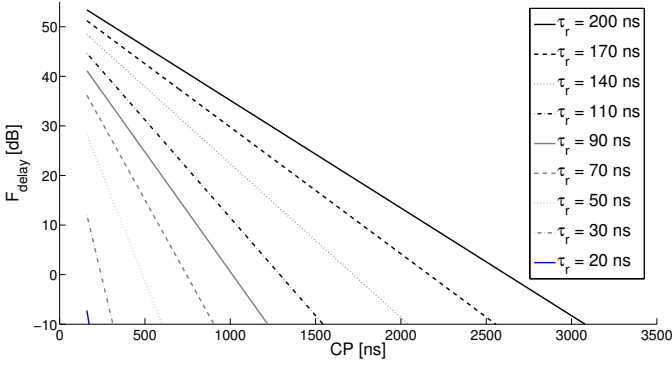


Figure 1. Calculated noise factor F_{delay} as a function of cyclic prefix CP for different reverberation time τ_r . This is based on IEEE 802.11a and a 20 dBm transmit power.

B. Influence of the FFT period P

We found that F_{delay} is inversely proportionally to P . In our analysis, the effect on the theoretical (transmission) data rate R_{data} (proportional to $P/(P + CP)$) and the hardware complexity (related to the number of used subcarriers, proportional to $BW \times P$) is taken into account simultaneously. A higher FFT period P would result in a lower performance loss due to delay spread (F_{delay}) as well as higher data rate, but the FFT processor would also require a higher size. When switching from $P = 3.2 \mu s$ to e.g., $6.4 \mu s$, F_{delay} would decrease with 3 dB and the data rate would increase with 11%. However, the FFT size would increase from 64 to 128. Therefore, increasing P is not really an efficient strategy to suppress the performance loss due to delay spread.

C. Influence of the bandwidth BW

Increasing the bandwidth results into an increased F_{delay} due to a reduced sampling period, which acts as an extension of the cyclic prefix. The dependency of F_{delay} on BW is rather slight. Comparing $BW = 160 \text{ MHz}$ (802.11ac) to 20 MHz , the increase of F_{delay} is only 3 dB for $\tau_r = 50 \text{ ns}$ and 2 dB for $\tau_r = 70 \text{ ns}$.

D. Influence of the sampling factor f_s

F_{delay} increases slightly for increasing f_s . E.g., when changing f_s from 1 to 4, there is an increase of F_{delay} by 0.6 dB for $\tau_r = 200 \text{ ns}$ and 2.5 dB for $\tau_r = 50 \text{ ns}$.

IV. IMPLICATIONS TO OFDM DESIGN

Our analysis shows that, to suppress the noise factor F_{delay} due to delay spread, an efficient strategy is related to the increase of the cyclic prefix length CP (i.e., guard interval (GI)). When switching to a long GI option of 1600 ns (from 800 ns GI), F_{delay} is reduced by even 17.4 dB for $\tau_r = 200 \text{ ns}$, and by 24.8 dB for $\tau_r = 140 \text{ ns}$. The data rate R_{data} is reduced by

17%, but this is largely compensated by the strong reduction of F_{delay} .

The strategy of an increased CP is easy with respect to the implementation, but the theoretical data rate R_{data} is reduced. To keep this data rate constant, the ratio between P and CP should be kept constant. As mentioned before, this requires a higher hardware complexity. However, in systems with a higher bandwidth mode, such as 802.11n (40 MHz) and 802.11ac (40/80/160 MHz), the more complex hardware could be combined with the principle of *scaled OFDM* [5]. This would provide a method for systems with a higher bandwidth mode to implement a long GI option for a lower bandwidth mode, without reduction of the (theoretical) data rate and without requiring a complex hardware extension.

V. CONCLUSION

In this work, the performance loss due to delay spread (in terms of F_{delay}) has been analyzed as a function of OFDM parameters for a wide range of the reverberation time (i.e., 10 – 200 ns). This loss, caused by diffuse multipath, can be severe: e.g., $F_{delay} = 38.6 \text{ dB}$ for $CP = 800 \text{ ns}$, a 30 dBm transmit power and a high (but realistic) $\tau_r = 140 \text{ ns}$. F_{delay} decreases exponentially with increasing CP . E.g., for $\tau_r = 140 \text{ ns}$, there is a reduction of F_{delay} by about 25 dB, when switching CP from 800 ns to 1600 ns. Further, we found that F_{delay} decreases inversely proportionally with increasing P . Taking into account the implications on the theoretical data rate and the hardware complexity, we propose to adopt a long guard interval option to the 802.11 OFDM standard to ensure reliable reception in high multipath environments. In future research, the analysis presented will be validated experimentally.

REFERENCES

- [1] F. Heereman, W. Joseph, E. Tanghe, L. Verloock, and L. Martens, "Performance degradation due to multipath noise for narrowband OFDM systems: Channel-based analysis and experimental determination," *IEEE Trans. Wireless Commun.* (submitted).
- [2] J. Andersen, J. Nielsen, G. Pedersen, G. Bauch, and M. Herdin, "Room electromagnetics," *IEEE Antennas and Propagation Magazine*, vol. 49, no. 2, pp. 27–33, 2007.
- [3] *IEEE Std 802.11n™-2009 amendment 5 to part 11: Wireless LAN Medium Access Control (MAC) and Physical Layer (PHY) specifications: enhancements for higher throughput*, IEEE Std., Oct. 2009.
- [4] "802.11ac technology introduction," Rohde & Schwarz, Tech. Rep., Mar. 2012.
- [5] *IEEE Std part 11: Wireless LAN Medium Access Control (MAC) and Physical Layer (PHY) specifications: Amendment 3: 3650-3700 MHz Operation in USA*, IEEE Std., Nov. 2008.